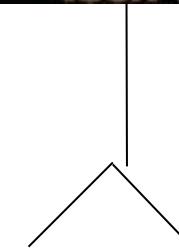


# MM Wave Injection Locked Frequency Dividers



Justin Heimerl

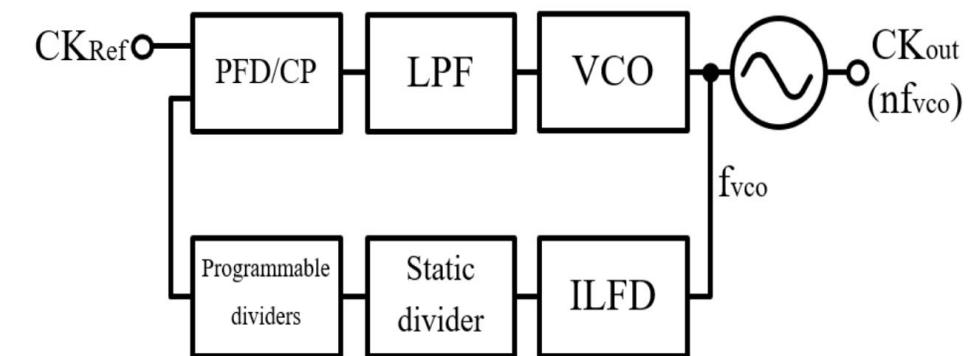
SiGe Devices and Circuits



# Who Needs Frequency Division?

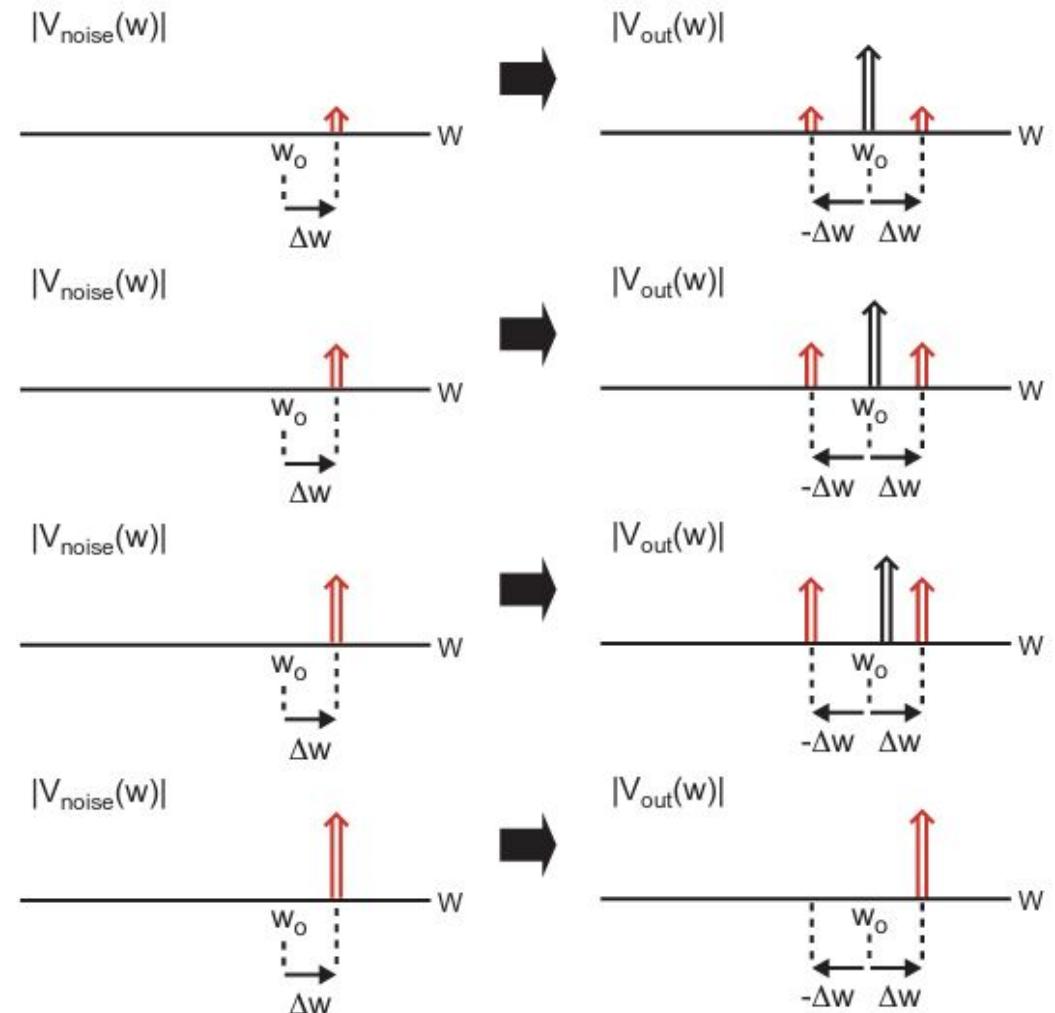
- Any multiplying PLL must use a frequency divider.
- Injection Locked Frequency Divider (ILFD) can be used as first divider.
  - Low DC power consumption.
  - High operation frequency (very viable at mm-wave frequencies).
  - Multiple division ratios.
  - Issue is locking range.

Divider Technique	Locking Range	DC Power	Operation Frequency	Division Ratio
ILFD	Low	Low	High	2,3, 4, 5
CML Divider	Very High	High	Low	$2^n$
Miller Divider	High	Medium	Medium - High	2



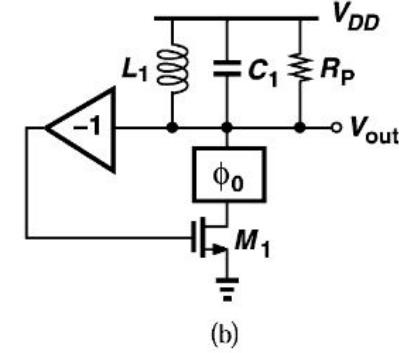
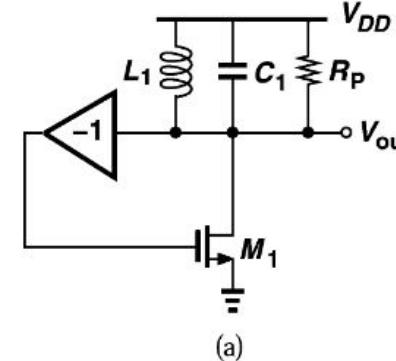
# Basics of Injection Locking

- Discovered in 17th century.
- Phenomenon present in all physical oscillating systems. (electronics, lasers, my cat's vocal cords around other cats)
- If two oscillators are coupled, and close in frequency, they will shift to oscillate at the same frequency.
- 



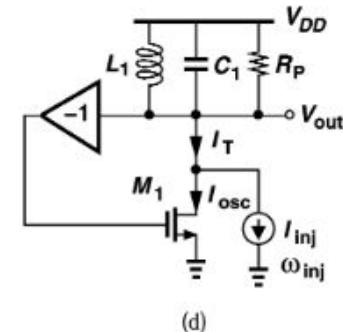
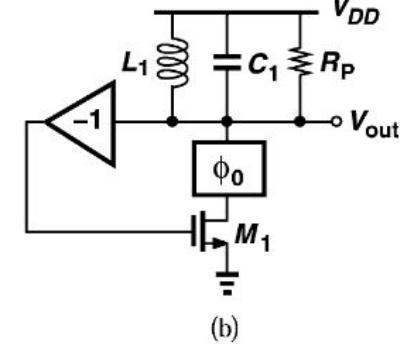
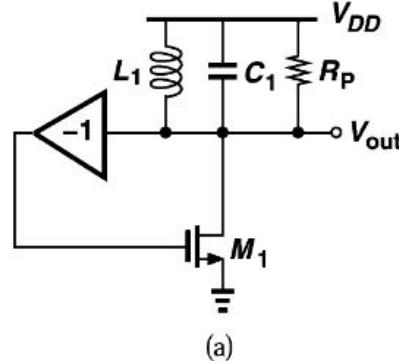
# Injection Locking in Electrical Oscillators

- Consider the LC oscillator in (a).
  - M1 is a CS device,  $180^\circ$  phase shift, inverter for another  $180^\circ$ .
  - What if a signal is injected off resonance?
  - Tank sees this off resonance current, gives a phase shift of  $\phi_0$ .
  - From Barkhausen criteria, how do we continue oscillating without  $360^\circ$  phase shift?



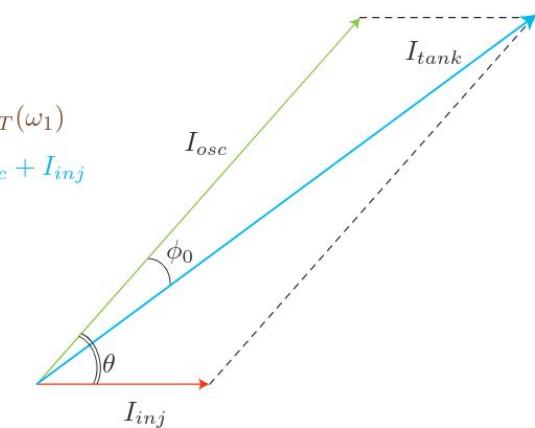
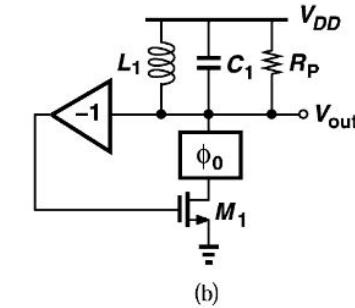
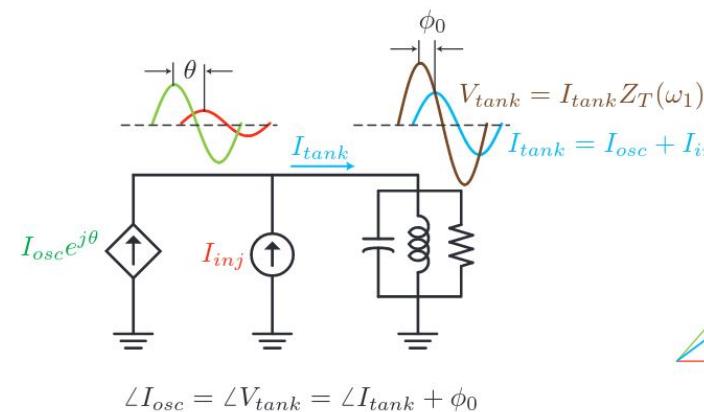
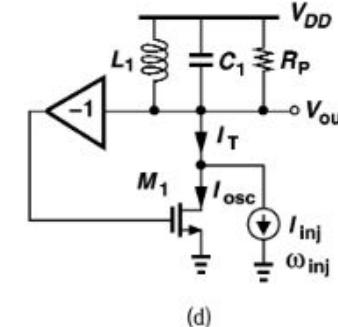
# Injection Locking in Electrical Oscillators

- This phase shift has to be compensated for somehow.
  - The compensation comes from the phase of the current losc and inj.



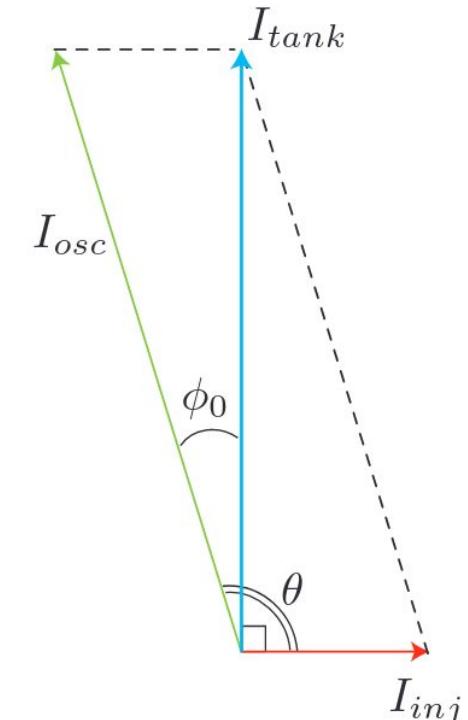
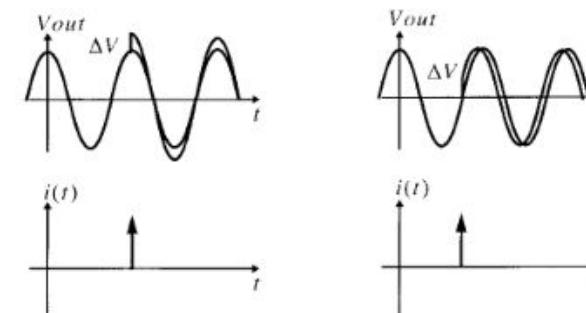
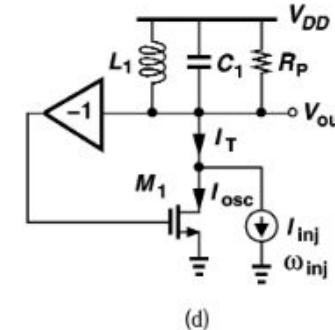
# Injection Locking in Electrical Oscillators

- This phase shift has to be compensated for somehow.
  - The compensation comes from the phase of the current  $I_{osc}$  and  $I_{inj}$ .
  - $I_{osc}$  is out of phase by  $\phi_0$  degrees with  $I_{tank}$ . As the injection frequency shifts, this phase difference also shifts.
  - This begs the question of how far can we drift until we can not lock anymore?



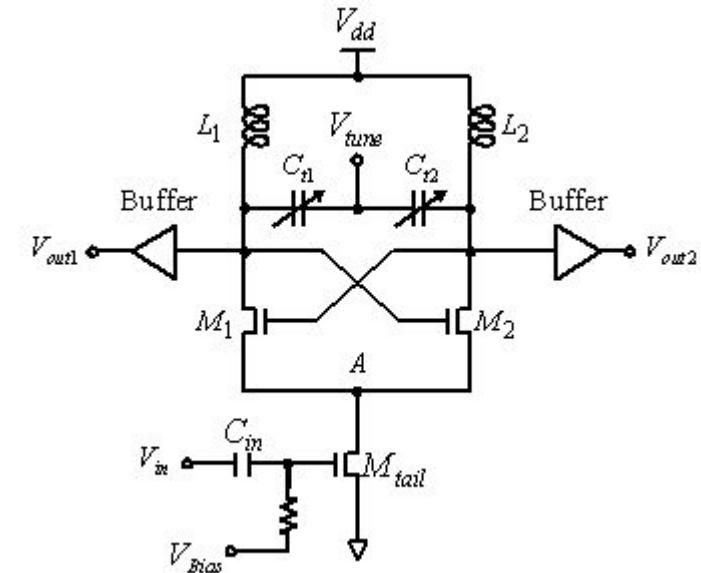
# Injection Locking in Electrical Oscillators

- We can use this information to determine the maximum locking range of the oscillator.
- Tank can only give up to  $90^\circ$  phase shift. When this happens the injected current is being injected at the peak of the tank current, and lock will not occur. (Impossible to produce  $d\phi/dt$  if signal is injected at peaks)



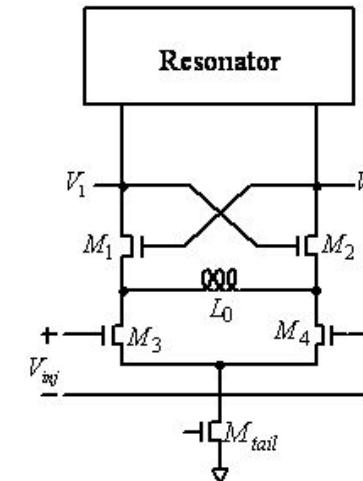
# Basics of Injection Locked Frequency Division

- Basic divide by 2 ILFD is shown.
  - Circuit has a second harmonic signal at node A.
  - Suppose  $V_{in}$  is close to this second harmonic. Node A will lock to  $V_{in}$ . Fundamental will also shift.
  - This accomplishes frequency division for some range of frequencies for which the output signal will lock.
  - Note the use of varactors.



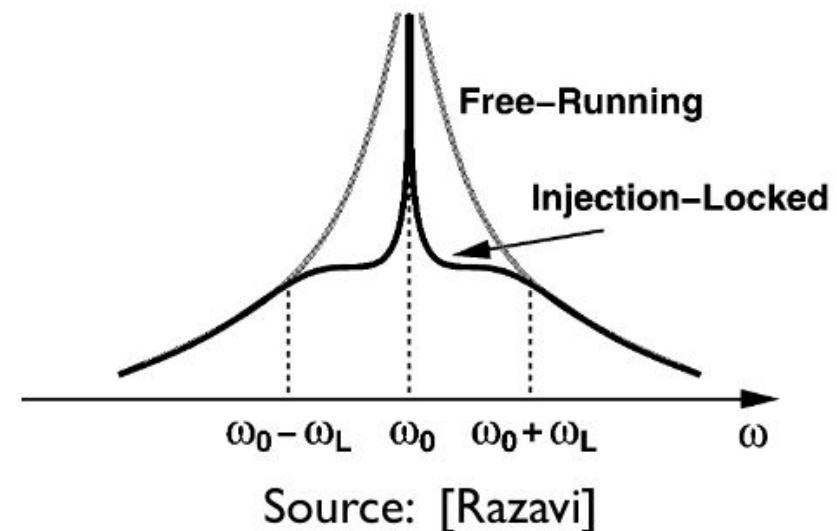
# Basics of Injection Locked Frequency Division

- Basic divide by 3 ILFD is shown.
  - Consider the half circuit of M3, M1, V1.
  - M1 now acts as a mixer, M3 injects current near 3rd (or any odd) harmonic.
  - The X-coupled pair is already oscillating, and thus has a second harmonic at the gate of M1. M1 thus mixes the injection current and 2nd harmonic, allowing one to move the fundamental present at V1.



# But What About Phase Noise?

- Phase noise actually improves compared to free running oscillator.
  - IF the input signal is clean.
  - IF the input signal is within the locking range of the divider.
    - Consider Hajimiri PN model. Where in the period the energy is injected matters.



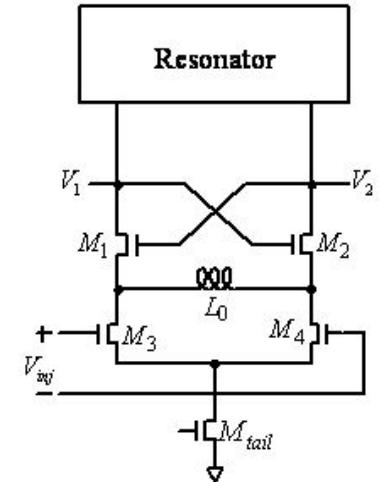
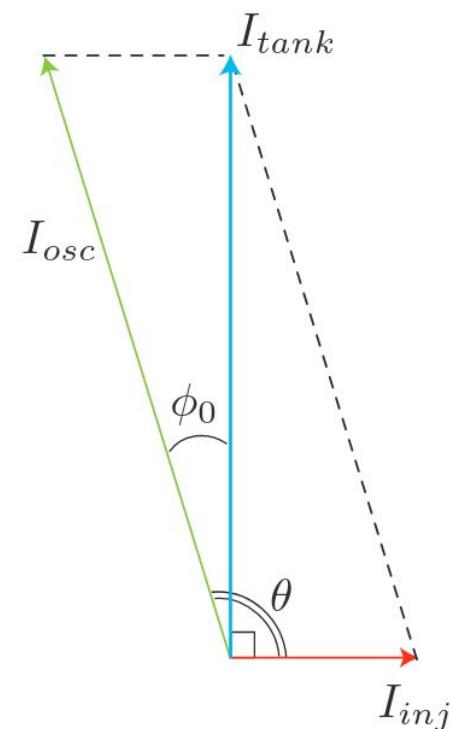
Source: [Razavi]

# Problem with Basic Topologies

- The 2nd harmonic here is very weak, resulting a low injection current.
- Increase locking range in 3 ways:
  - Lower Q (bad for phase noise)
  - Decrease oscillation amplitude (also bad for phase noise and output power)
  - Increase injection current (best approach)

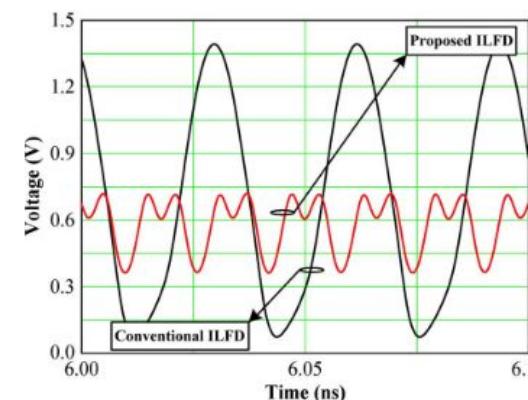
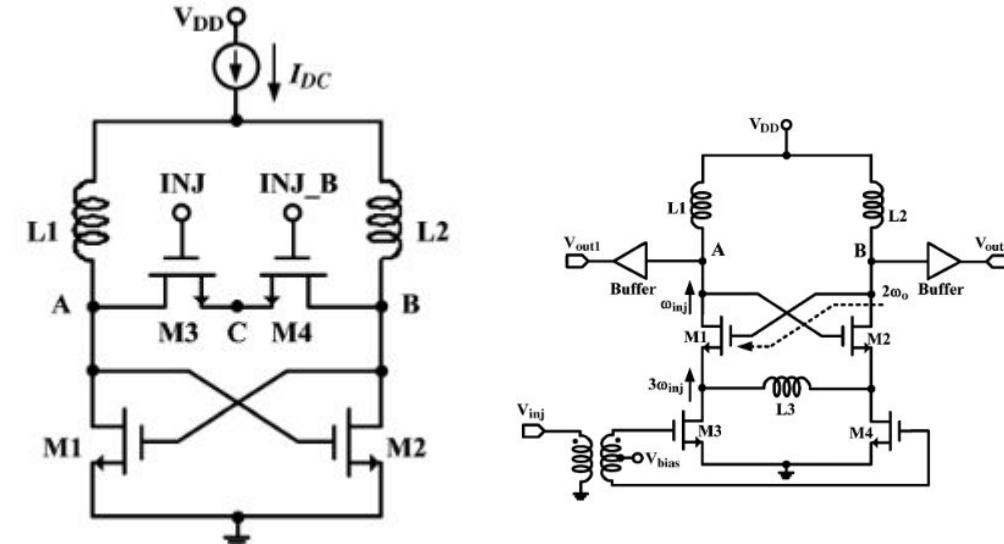
$$(\omega_0 - \omega_{inj}) = \frac{\omega_0}{2Q} \frac{I_{inj}}{I_{osc}} \frac{1}{\sqrt{1 - \frac{I_{inj}^2}{I_{osc}^2}}}$$

Maximum Locking Range



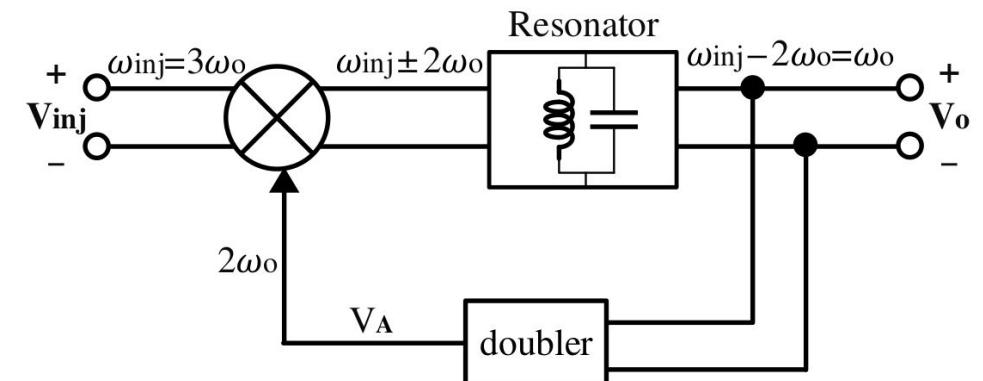
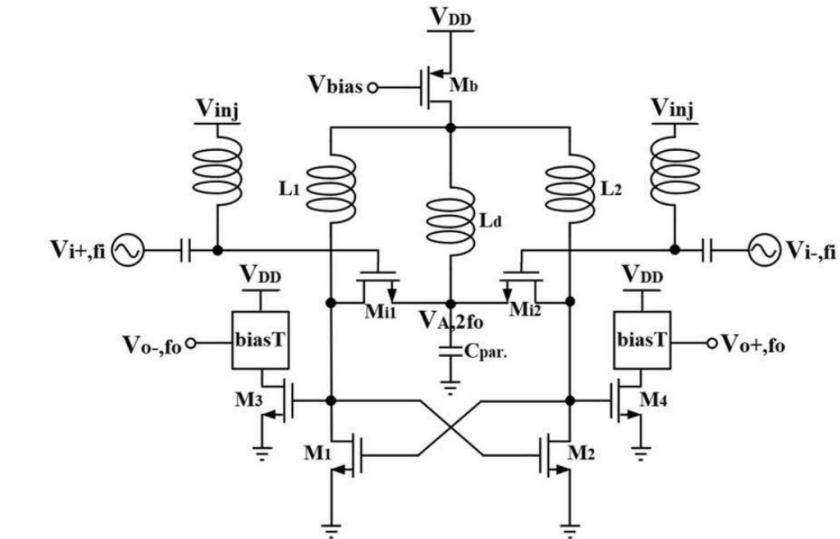
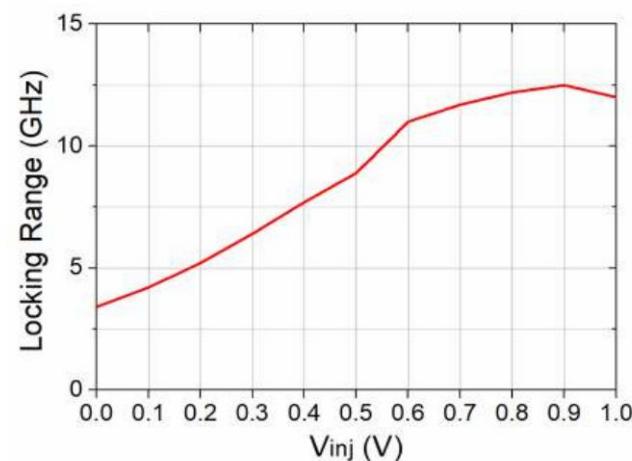
# Isolate Second Harmonic

- Simply floating node C allows for an increase in locking range while paying no power penalty.
- This method can increase 2nd harmonic power by  $\sim 8\text{dB}$ .
- Authors also recommend larger device size to de-Q the tank, increase injection current.



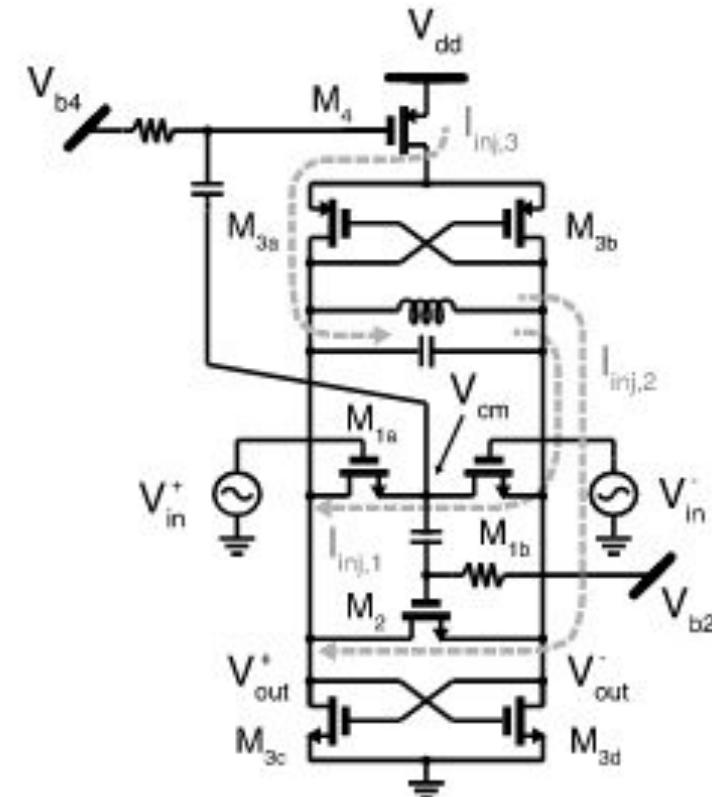
# Second Harmonic Boosting

- Second harmonic amplitude can also be boosted to increase injection current.
  - Simply resonate the second harmonic using  $L_d$ , resonates with routing capacitance at  $2f_o$ .
  - 14% locking range at 80 GHz



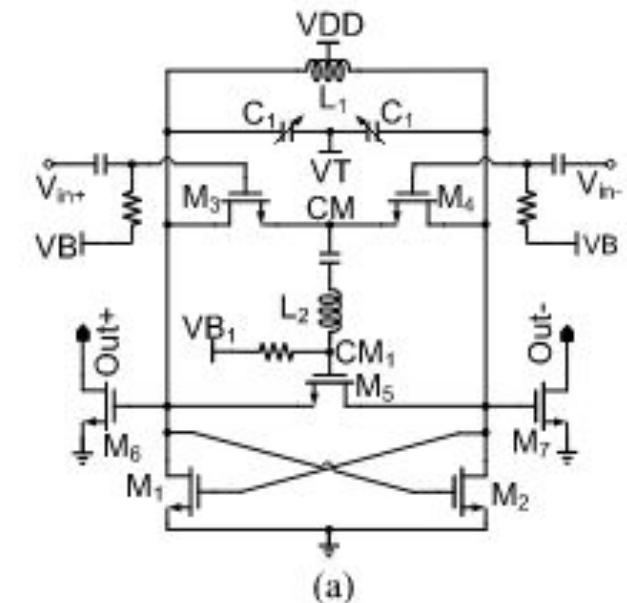
# Second Harmonic Utilization

- Utilizing the second harmonic is the clearest way to increase the injection current, increasing locking range.
- Try to use the second harmonic to boost injection current.
  - Floating the source/drain of the injection devices causes large 2nd harmonic.
  - This harmonic is used as a mixing input into M2, dividing it by 2, increasing the injection current at baseband.
  - 4th harmonic also contributes, but minimally.
  - 23% locking range at 14 GHz



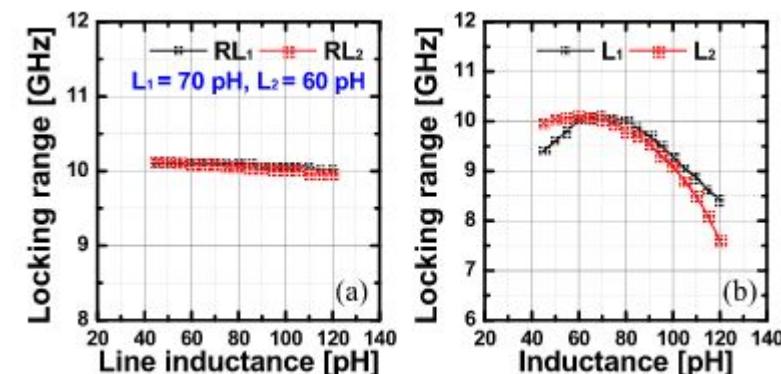
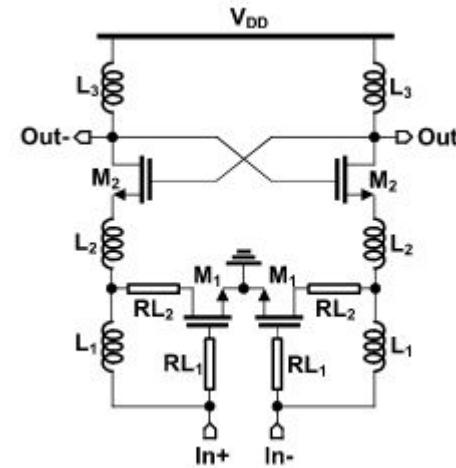
# Why not Both?

- Resonate second harmonic with routing and device parasitics (using L2 here).
  - CM1 node oscillating at the second harmonic, OUT +/- is at baseband, so mixing occurs.
  - Filter so linj is at baseband, boost locking range.
  - ~20% locking range at 30 GHz.



# What about Feedback?

- L1 used to feedback 2 and 3 for signals, L2 used as peaking inductor.
  - Achieves 10% locking range at W band, uses 7.8mW.
  - Inductor/filter design has a large effect on locking range.
  - Combining this approach with other approaches might have merit. Utilize second harmonic present at output signal and feedback to mixer?



- Injection locking is a useful idea for frequency synthesis.
- Having access to a divide by three stage is useful in PLL design.
  - If divide by two is sufficient a Miller topology is probably better.
- Most ideas center around utilizing the second harmonic at the common node of the mixers.
- Locking ranges at W band are generally from 10-15% for state of the art.
- Power draw ranges from 1-10 mW for state of the art.
- Lower Q can increase lock range, but you might pay PN penalty.
- Hopefully Sunil isn't shaking his head too hard by this point

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- Can some transmission line based approach be used to further isolate 2nd harmonic?
  - TL in between mixing devices? Short for  $f_0$ , open for  $2f_0$ ?
- Can some sort of feedback or amplifier approach be used to boost second harmonic?
- Better approach to switch/mixer in these topologies?